

AOS 801: Advanced Tropical Meteorology  
Lecture 3 Spring 2023  
Moist Thermodynamics

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Photo courtesy of Haochang Luo

# Announcements

Homework 1 will be assigned on Monday.

In the meantime, please review all the material we've covered so far. It's a lot!

I will upload several class notes to help you with the review.

[http://tropic.ssec.wisc.edu/real-time/mtpw2/product.php?  
color\\_type=tpw\\_nrl\\_colors&prod=global2&timespan=24hrs&anim=html5](http://tropic.ssec.wisc.edu/real-time/mtpw2/product.php?color_type=tpw_nrl_colors&prod=global2&timespan=24hrs&anim=html5)

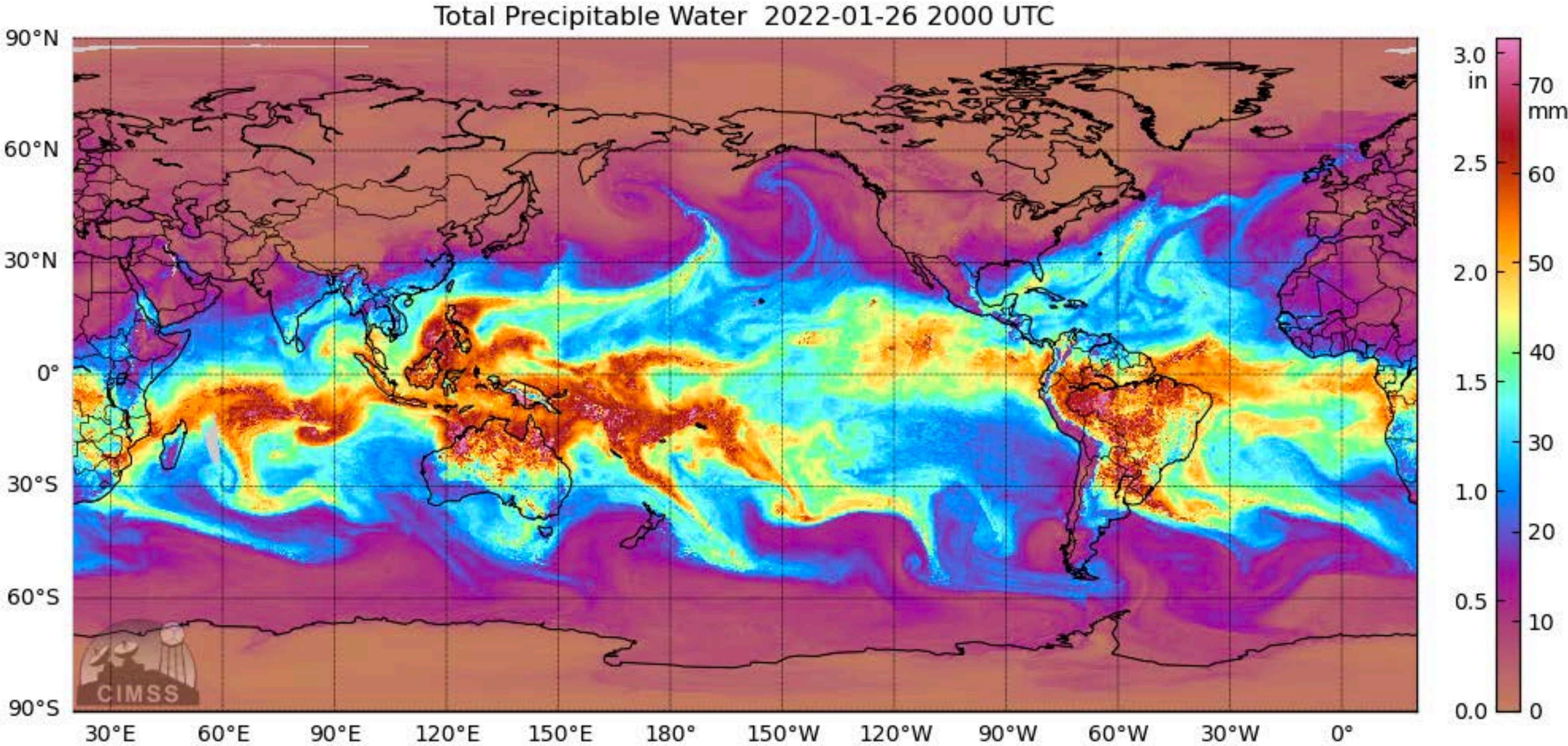
[https://a.atmos.washington.edu/~ovens/wxloop.cgi?ir\\_moll+/14d/](https://a.atmos.washington.edu/~ovens/wxloop.cgi?ir_moll+/14d/)

[https://www.cpc.ncep.noaa.gov/products/precip/CWlink/ir\\_anim\\_monthly.shtml](https://www.cpc.ncep.noaa.gov/products/precip/CWlink/ir_anim_monthly.shtml)

[https://www.cpc.ncep.noaa.gov/products/precip/CWlink/MJO/obs\\_phase40\\_small.gif](https://www.cpc.ncep.noaa.gov/products/precip/CWlink/MJO/obs_phase40_small.gif)

# Column water vapor

$$\langle q \rangle = \frac{1}{g} \int_0^{p_s} q dp = \int_0^\infty \rho q dz$$



# Convection $Q_c$

To understand convection we must invoke the equation for conservation of moisture



$$\frac{Dq}{Dt} = S_q$$

$$S_q = e - c + s - d - \frac{\partial F_q}{\partial p}$$

e = evaporation

c = condensation

s = sublimation

d = deposition

$F_q$  Turbulent flux of moisture

$$\frac{Dq}{Dt} = S_q$$

$$S_q = \boxed{e} - c + s - d - \boxed{\frac{\partial F_q}{\partial p}}$$

Includes only evaporation that happens within the parcel

Includes evaporation that occurs as a result of turbulent mixing with a surface of water

# Convection $Q_c$

Need to go back to 1st law to account for condensation

$$C_p \frac{DT}{Dt} = Q + \alpha \frac{Dp}{Dt}$$

$$\frac{Dq}{Dt} = S_q$$

Latent heat is released during condensation

$$Q_c \simeq L_v(c - e)$$

$$S_q \simeq e - c$$

So our heating is negatively related to changes in moisture

$$Q_c \simeq -L_v \frac{Dq}{Dt}$$

# The equivalent potential temperature

Need to go back to 1st law to account for condensation

$$C_p dT = -L_v dq_v + \alpha dp$$

Can be written as

$$C_p T d \ln \theta = -L_v dq_v$$

Which can be solved to obtain

$$\theta_e \simeq \theta \exp \left( \frac{L_v q_v}{C_p T} \right)$$

$$\frac{Dq_v}{Dt} = S_q$$

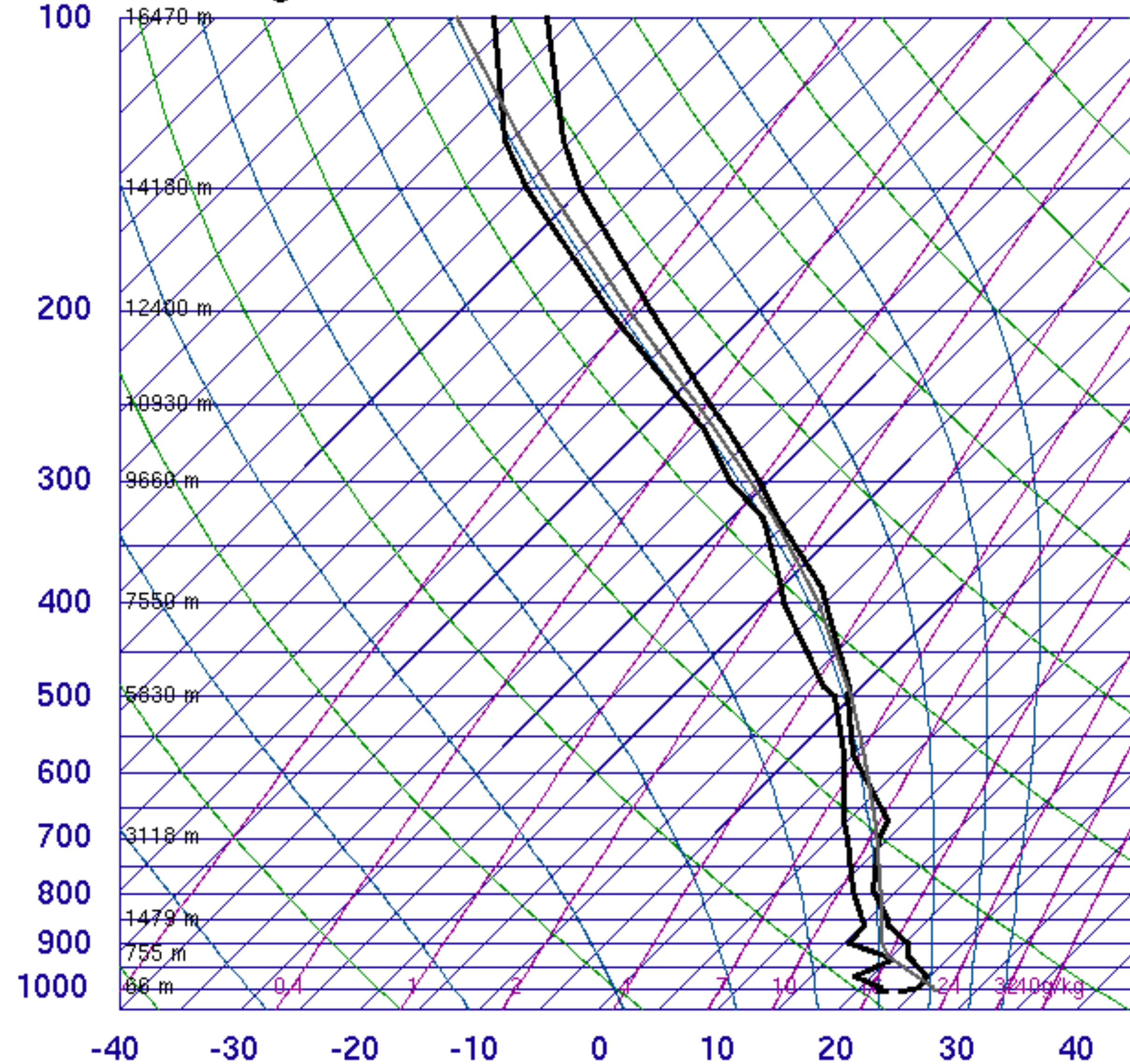
$$S_q = e - c$$

## The equivalent potential temperature

The temperature a parcel would have if it condensed all its water vapor and was brought to the surface adiabatically



# 96253 WIPL Bengkulu



SLAT	-3.88
SLON	102.33
SELV	16.00
SHOW	1.20
LIFT	-0.24
LFTV	-0.33
SWET	249.2
KINX	34.00
CTOT	19.90
VTOT	22.10
TOTL	42.00
CAPE	46.76
CAPV	69.08
CINS	-49.8
CINV	-42.0
EQLV	490.9
EQTV	465.5
LFCT	823.9
LFCV	837.2
BRCH	2.60
BRCV	3.84
LCLT	292.2
LCLP	917.5
LCLE	344.5
MLTH	299.5
MLMR	15.42
THCK	5764.
PWAT	58.11

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# Moist entropy

**We can define the moist entropy that is** using the following form of the first law

$$C_p T d \ln \theta + L_v dq_v = 0$$

Dividing the equation by T yields and rearranging the terms yields the following

$$ds_m = d \left( C_p \ln \theta + \frac{L_v q_v}{T} \right) \quad s_m = C_p \ln \theta_e + \text{const}$$

**The specific moist entropy**

# Moist entropy budget

In deriving the equiv. potential temperature and moist entropy we assumed that

$$Q \simeq L_v(c - e) \qquad dq_v \simeq e - c$$

This is not true. There are multiple sources and sinks of these variables. Hence they are not conserved.

$$\frac{Ds_m}{Dt} = \frac{\dot{Q}_e}{T} \quad \text{Where} \quad \dot{Q}_e = -L_f(m - f + s - d) + \dot{Q}_r + -\frac{\partial}{\partial p}(F_q + F_T)$$

e = evaporation  
c = condensation  
s = sublimation  
d = deposition  
m = melting  
f = freezing

# The moist static energy budget

$$C_p \frac{DT}{Dt} - \alpha \frac{Dp}{Dt} = -L_v \frac{Dq_v}{Dt} + \dot{Q}_e$$

We can get a simpler conserved variable if we assume hydrostatic balance:

$$\frac{Dp}{Dt} \simeq \frac{dp}{dz} \frac{Dz}{Dt} = -\rho g \frac{Dz}{Dt} = -\rho \frac{D\Phi}{Dt}$$

In HW1 you will examine the validity of this approximation.

Which we can plug into the first equation above to obtain

$$\frac{DMSE}{Dt} = \dot{Q}_e \quad \text{Where} \quad MSE = c_p T + \Phi + L_v q_v$$

**The moist static energy**

# Relationship between MSE and moist entropy

Given that

$$\frac{Ds_m}{Dt} = \frac{\dot{Q}_e}{T} \quad \text{and} \quad \frac{DMSE}{Dt} = \dot{Q}_e$$

It follows that

$$\frac{Ds_m}{Dt} = \frac{1}{T} \frac{DMSE}{Dt} \quad Tds_m = dMSE$$

Also recall that

$$ds_m = C_p d \ln \theta_e$$

The **MSE**, **moist entropy** and  $\theta_e$  are interrelated

# Maxwell's Relation

We can obtain several relations using MSE or moist entropy that will prove useful in this class

$$Tds_m = d\text{MSE} = C_p dT + d\Phi + L_v dq$$

If we keep pressure constant:

$$T(ds_m)_p = C_p dT + L_v dq = (d\varepsilon_m)_p$$

If moist entropy is kept constant

$$(d\varepsilon_m)_{s_m} = \alpha(dp)_{s_m}$$

Cross differentiation yields

$$\left(\frac{dT}{dp}\right)_{s_m} = \left(\frac{d\alpha}{ds}\right)_p$$

# The moist adiabatic lapse rate

A parcel that rises moist adiabatically conserves its MSE as it rises

$$\frac{DMSE}{Dz} \approx 0$$

By expanding the definition and after some algebra and rearranging, we can obtain the moist adiabatic lapse rate

$$\frac{dT}{dz} = -\Gamma_m \quad \Gamma_m = \Gamma_d \frac{1 + \frac{L_v q_s}{R_d T}}{1 + \frac{L_v^2 q_s}{c_p R_v T^2}} \quad \Gamma_d = \frac{g}{C_p}$$

Is the **moist adiabatic lapse rate**.